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(54) **A process for producing a shape-selective, metal-containing catalyst and use thereof in hydrocarbon conversion processes**

Verfahren zur Herstellung eines formselektiven, metall-enthaltenden Katalysators; seine Verwendung in der Umwandlung von Kohlenwasserstoffen

Préparation de catalyseurs à sélectivité de forme et contenant des métaux; leur utilisation dans la conversion d'hydrocarbures

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Description

[0001] The invention relates to a process for producing a shape-selective metal-containing molecular sieve catalyst and to the use of such a catalyst shape-selective hydrocarbon conversion processes.

[0002] The term shape-selective catalysis describes unexpected catalytic selectivities in molecular sieves and particularly zeolites. The principles behind shape selective catalysis have been reviewed extensively, e.g., by Chen NY, Garwood WE, and Dwyer FG, *Shape Selective Catalysis In Industrial Applications*, Marcel Dekker, Inc., New York (1989). Within a zeolite pore, hydrocarbon conversion reactions such as paraffin isomerization, olefin skeletal or double bond isomerization, oligomerization, and aromatic disproportionation, alkylation, or transalkylation reactions are governed by constraints imposed by the channel size. Reactant selectivity occurs when a fraction of the feedstock is too large to enter the zeolite pores to react. Product selectivity occurs when some of the products cannot leave the zeolite channels. Product distributions can also be altered by transition state selectivity in which certain reactions cannot occur because the reaction transition state is too large to form within the zeolite pores or cages. Another type of selectivity results from configurational diffusion where the dimensions of the molecule approach that of the zeolite pore system. A small change in dimensions of the molecule or the zeolite pore can result in large diffusion changes leading to different product distributions. This type of shape selective catalysis is demonstrated, for example, in selective disproportionation of toluene to *para*-xylene.

[0003] *Para*-xylene is a very valuable commercial product useful in the production of polyester fibers. The catalytic production of *p*-xylene has received much attention in the scientific community and various methods for increasing catalyst *para*-selectivity have been described.

[0004] One method by which the *para*-selectivity of a molecular sieve catalyst can be improved is by modifying the catalyst through treatment with "selectivating agents". For example, modification methods have been suggested wherein the catalyst is modified by treatment prior to use to provide a silica coating. Thus, U.S. Patent Nos. 4,477,583 and 4,127,616 disclose methods wherein a catalyst is contacted at ambient conditions with a modifying compound such as phenylmethylsilicone in a hydrocarbon solvent or an aqueous emulsion, followed by calcination. More recently, an *in-situ* silicon selectivation process has been described in U.S. Patent No. 5,498,814 in which a reaction stream comprising toluene, hydrogen and an organosilicon compound is contacted with a molecular sieve under toluene conversion conditions and, when the *para*-selectivity of the catalyst has been increased to at least 90% based on the C_8 products, the organosilicon feed is discontinued and the selectivated catalyst is used to effect *para*-selective disproportionation of the toluene. It is also known from, for example, U.S. Patent No. 4,097,543 to effect selectivation of zeolite catalysts by coking and from U.S. Patent No. 5,625,103 by a combination of silica deposition and coking.

[0005] For many hydrocarbon conversion processes it is desirable to provide a catalyst which not only exhibits both shape selectivity but also contains a hydrogenation-dehydrogenation metal function. For example, in toluene disproportionation and xylene isomerization, shape selectivity in the catalyst is important to enhance the production of the valuable *para*-xylene product, whereas hydrogenation-dehydrogenation functionality is desirable to remove ethylbenzene in the product and/or the feed. There is, however, a problem in producing a catalyst which exhibits both of these properties in that it is often found that the hydrogenation-dehydrogenation functionality is of limited stability when present in a catalyst which has selectivated by existing techniques.

[0006] According to the invention, there is provided a process according to claim 1 for producing a shape-selective, metal-containing catalyst comprising the steps of:

(a) incorporating a hydrogenation-dehydrogenation metal into a molecular sieve catalyst to provide a metal-containing catalyst, and

(b) gradient selectivating the metal-containing catalyst under an *in situ* selectivation protocol that comprises a progressive temperature gradient to provide a shape-selective, metal-containing catalyst.

[0007] Using an *in-situ* selectivation process in which the temperature is gradually increased during selectivation is found to produce a catalyst in which the hydrogenation-dehydrogenation function has enhanced stability in hydrocarbon conversion processes.

[0008] The progressive temperature gradient includes a lower temperature of 350° to 460°C, and an upper temperature of 420° to 550°C. More preferably, the lower temperature is from 380° to 430°C and the upper temperature is from 450° to 510°C. Moreover, the *in situ* selectivation protocol preferably further comprises a pressure of from 100 to 14,000 kPa (0 to 2000 psig), a H_2/HC mole ratio of up to 20, and a WHSV of from 0.1 to 100 hr⁻¹.

[0009] The catalyst can also have been further modified by preselectivating the catalyst, i.e., by exposing the catalyst to at least one preselectivation sequence, each preselectivation sequence comprising contacting the catalyst with an organosilicon compound and then calcining the contacted catalyst.

[0010] The invention also resides in a hydrocarbon conversion process over a shape-selective, metal-containing catalyst produced according to the process of one aspect of the invention method.

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Catalyst System

[0011] Catalysts useful in this invention comprise catalytic molecular sieves, such as zeolites. Preferably, the zeolite employed is preferably an intermediate pore size zeolite, particularly a pore size of from 5 Å to 7 Å. One measure of zeolite pore size is Constraint Index which is described in U.S. Patent No. 4,016,218. Suitable intermediate pore size zeolites for use in the invention have a Constraint Index within the approximate range of 1 to 12. Examples of intermediate pore size zeolites useful in this invention include ZSM-5 (U.S. Patent No. 3,702,886 and Re. 29,948); ZSM-11 (U.S. Patent No. 3,709,979); ZSM-12 (U.S. Patent No. 3,832,448); ZSM-22 (U.S. Patent No. 4,556,447); ZSM-23 (U.S. Patent No. 4,076,842); ZSM-35 (U.S. Patent No. 4,016,245); ZSM-48 (U.S. Patent No. 4,397,827); ZSM-57 (U.S. Patent No. 4,046,685); and ZSM-58 (U.S. Patent No. 4,417,780). ZSM-5 is particularly preferred.

[0012] The suitable molecular sieve may be employed in combination with a support or binder material such as, for example, a porous inorganic oxide support or a clay binder. For example, it may be desirable to formulate the catalyst of the invention with another material resistant to the temperature and other conditions of the hydrocarbon conversion process. Illustrative examples of binder materials include synthetic or naturally occurring substances as well as inorganic materials such as clay, silica, and/or metal oxides, such as alumina, vanadia, beryllia, thorla, magnesia, titania, zirconia, borla, and combinations thereof. The preferred binder is primarily silica. The metal oxides may be naturally occurring or in the form of gelatinous precipitates or gels including mixtures of silica and metal oxides.

[0013] Naturally occurring clays that can be composited with the zeolite include those of the montmorillonite and kaolin families, which families include the subbentonites and the kaolins commonly known as Dixie, McNamee, Georgia, and Florida clays, or others in which the main mineral constituent is halloysite, kaolinite, dickite, nacrite, or anauxite. Suitable clay materials include, by way of example, bentonite and kieselguhr. Such clays can be used in the raw state as originally mined or initially subjected to calcination, acid treatment, or chemical modification.

[0014] The relative proportion of suitable crystalline molecular sieve to the total composition of catalyst and binder or support may be from 1 to 99 wt.%, preferably from 30 to 90 wt.%, and more preferably from 50 to 80 wt.%, of the composition.

Hydrogenation-Dehydrogenation Functional Modification

[0015] A hydrogenation-dehydrogenation functional metal is incorporated into the catalyst of the invention. Such metals are known in the art to reduce ethylbenzene by-product in hydrocarbon conversion processes, such as toluene disproportionation (see U.S. Patent No. 5,498,814).

[0016] Any metal possessing the desired hydrogenation-dehydrogenation function can be used in the process of the invention. Examples of such functional metals include the oxide, hydroxide, sulfide, or free metal (i.e., zero valent) forms of metals in the Groups 3 to 15 of the periodic table. Preferred metals include Group 8, 9, and 10 metals (i.e., Pt, Pd, Ir, Rh, Os, Ru, Ni, Co, and Fe), Group 7 metals (i.e., Mn, Tc, and Re), Group 6 metals (i.e., Cr, Mo, and W), Group 15 metals (i.e., Sb and Bi), Group 14 metals (i.e., Sn and Pb), Group 13 metals (i.e., Ga and In), Group 11 metals (i.e., Cu, Ag, and Au), and Group 12 metals (i.e., Zn, Cd, and Hg). Noble metals (i.e., Pt, Pd, Ir, Rh, Os, Re, Ru, Mo, and W) may be desirable for use. Preferred functional metals include, for example, cadmium, cobalt, copper, gold, iron, mercury, molybdenum, nickel, osmium, palladium, platinum, rhenium, rhodium, ruthenium, silver, zinc, and mixtures thereof. Platinum is a highly preferred functional metal according to this invention.

[0017] Combinations or mixtures of catalytic forms of such noble or non-noble metals, such as combinations of Pt with Sn, may be used. The valence state of the metal is preferably reduced, e.g., when this component is in the form of an oxide or hydroxide. The reduced valence state of the functional metal may be attained, *in situ*, during the course of a reaction, when a reducing agent, such as hydrogen, is included in the feed to the reaction.

[0018] The functional metal may be incorporated into the catalyst by methods known in the art, such as ion exchange, impregnation, or physical admixture. For example, solutions of appropriate metal salts may be contacted with the remaining catalyst components under conditions sufficient to combine the respective components. The metal-containing salt is preferably water-soluble. Examples of such salts include chloroplatinic acid, tetraammine platinum complexes, platinum chloride, tin sulfate, and tin chloride. The metal may be incorporated in the form of a cationic, anionic, or neutral complex such as $\text{Pt}(\text{NH}_3)_4^{2+}$, and cationic complexes of this type will be found convenient for exchanging metals onto the zeolite. Anionic complexes such as the vanadate or metatungstate ions are also useful for impregnating metals into the zeolites. Incorporation is preferably undertaken in accordance with the method described in U.S. Patent No. 4,312,790. After incorporation of the metal, the catalyst can then be filtered, washed with water, and calcined at temperatures of 250° to 500°C.

[0019] The functional metal must be able to enter the pores of the catalyst, i.e., permeate into the catalyst, to be able to survive high temperature exposure, such as that associated with calcination or conversion conditions. Addition of the metal can be accomplished through mixing the catalyst with a solution, preferably aqueous, of an appropriate metal salt. The mixing can be performed at about ambient temperature or at elevated temperatures, e.g., through reflux. In

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certain circumstances several exchanges may be required to facilitate proper permeation of the desired metal. For example, in the case of an acidic form of a catalyst, e.g., HZSM-5, it may be desirable to perform first exchange to provide an ammonium form, i.e., $\text{NH}_4\text{-HZSM-5}$, with a second exchange to provide the metal form.

[0020] The amount of functional metal may be that amount which increases the catalytic ability of the overall catalyst to catalytically hydrogenate or dehydrogenate an organic compound, e.g., ethylene, under sufficient hydrogenation or dehydrogenation conditions. This amount is referred to herein as a catalytic amount. The amount of the functional metal is suitably from 0.001 to 10 wt.%, preferably from 0.05 to 5 wt.%, more preferably from 0.1 to 2 wt.%, based on the total weight of the modified catalyst. However it will be recognized that the required amount of the functional metal will vary with the nature of the component, with less of the highly active noble metals, particularly platinum, being required than of the less active base metals.

[0021] As noted above, the hydrogenation-dehydrogenation function provided by the functional metal can decrease the ethylbenzene by-product in hydrocarbon conversions. However, it has been observed with conventional functional metal-modified catalysts that ethylbenzene yield gradually increases as a function of time on stream (TOS). This is not completely understood, but is believed to be associated with a gradual migration of the functional metal out of the catalyst pores to the surface of the catalyst, where its functionality is lost. It has now been found that such gradual increase in ethylbenzene in the catalyst effluent can be substantially inhibited by using the method of the invention. It is believed that this observation may be associated with a substantial inhibition of the migration of the functional metal out of the catalyst that would otherwise occur with increasing time on stream.

Catalyst Selectivation

[0022] One known method of selectivating of a molecular sieve catalyst, called "*ex situ* selectivation" or "preselectivation," involves subjecting the catalyst to one or more treatments with a silicon compound in a liquid carrier, each treatment being followed by calcination of the treated catalyst in an oxygen-containing atmosphere, e.g., air. Thus, the zeolite, e.g., HZSM-5, is treated at least once, preferably at least twice, with a fluid medium comprising a silicon compound and a carrier fluid. The carrier fluid is then removed, e.g., evaporated, leaving a deposited residue of the silicon compound on the catalyst. Subsequently, the coated catalyst is calcined to convert the silicon-containing material to a silica material. Such a method is described in, for example, U.S. Patent Nos. 5,478,823 and 5,403,800.

[0023] Another known method of selectivation of a molecular sieve catalyst is performed with the catalyst in the reactor used for a subsequent hydrocarbon conversion reaction and is normally termed *in situ* selectivation. Such a selectivation process is described in, for example, U.S. Patent No. 5,488,814. The process of the invention employs *in situ* selectivation, either alone or in combination with *ex situ* selectivation.

[0024] Known *in situ* selectivation protocols include passing a feed stream comprising hydrogen and an aromatic (e.g., toluene) or a paraffin (e.g., hexane or decane) and an organosilicon compound over the zeolite under "*in situ* selectivation conditions," i.e., conditions sufficient to deposit a residue of the organosilicon compound on the zeolite. Suitable organosilicon compounds include volatile organosilicon compounds having sufficient vapor pressure for proper deposition under *in situ* selectivation conditions. Toluene may comprise 50 to 100 wt.%, e.g., at least 80 wt.%, of the hydrocarbons in the feedstock. Other hydrocarbons, such as benzene, xylenes and trimethylbenzenes, may also be present in the feedstock for *in situ* selectivation.

[0025] *In situ* selectivation protocols typically comprise conditions include temperatures ranging from 100° to 800°C, preferably from 300° to 500°C; pressures ranging from 100 to 14,000 kPa (0 to 2000 psig, preferably from 200 to 5,600 kPa (15 to 800 psig); a H_2/HC mole ratio up to 20, preferably from 1 to 4; at a WHSV of from 0.1 to 100 hr^{-1} , preferably from 0.1 to 10 hr^{-1} . Upon thermolysis, a siliceous coating is deposited on the zeolite surface, eliminating surface activity and enhancing shape-selectivity.

[0026] The presence of a sufficient amount of hydrogen in the *in situ* selectivation feedstock is important to prevent rapid aging of the catalyst during the selectivation process resulting in an excessive reduction in the catalyst activity, possibly accompanied by a reduction in selectivity for ethylbenzene conversion. This rapid aging is believed to result from a rapid build-up of excessive amounts of carbonaceous deposits (i.e., coke), which may even extend into the pore system of the zeolite in the catalyst. However, even when hydrogen is used in optimal fashion to prevent aging during the selectivation process, a small amount of carbonaceous deposits forms on the catalyst. As a result of this carbonaceous deposit, the elemental analysis of the *in situ* selectivated catalyst reveals a carbon content significantly greater than the carbon content of the fresh catalyst prepared by the multiple impregnation method described herein. More particularly, the *in situ* selectivated catalyst may contain at least 2 wt.%, e.g., at least 4 wt.%, of carbon by elemental analysis, whereas the catalyst prepared by the multiple impregnation method may contain less than 0.5 wt.% of carbon as measured by elemental analysis. These weight percentages are expressed in terms of the weight of the entire catalyst including the zeolite, binder, and optional components, e.g., hydrogenation-dehydrogenation components.

[0027] The gradient selectivation protocol used in the present invention differs from conventional *in situ* selectivation in that conventional *in situ* selectivation is performed under conditions that accommodate efficient hydrocarbon con-

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version. Typically, an *in situ* selectivation temperature is established that substantially corresponds to a nominal conversion temperature, and an *in situ* selectivating agent is added to the hydrocarbon feed. At a later time, the *in situ* selectivating agent feed is stopped while the hydrocarbon conversion is continued. By contrast, the gradient selectivation protocol according to the invention requires a controlled modulation of conversion temperature marked by imposition of a temperature gradient during the period in which the selectivating agent is co-fed to the reactor. By this is meant that, for a substantial portion of the *in situ* selectivation period, the catalyst is exposed to a temperature gradient wherein the temperature is raised from a lower temperature to a higher temperature. The gradient may be continuous, semi-continuous, or stepped. If stepped, the gradient may have at least one intermediate temperature step, and preferably two or more temperature steps, at which the temperature is maintained for a period of time before being raised. Typically, stepped gradients are easier to control, and they are for this reason preferred.

[0028] Once the gradient is completed, the selectivating agent feed is terminated and the temperature is adjusted to the nominal conversion temperature whereupon the hydrocarbon conversion process is allowed to proceed. Other conversion parameters, e.g., space velocity, hydrogen content, pressure, etc., may be adjusted as needed following the gradient selectivation.

[0029] The lower and upper temperature levels of the temperature gradient will depend upon the nature of the hydrocarbon conversion, as different conversion processes require different nominal conversion conditions for optimized yields. However, the temperature gradient will generally traverse a range of 15° to 150°C, preferably 25° to 100°C. The lower temperature level may be from 350° to 460°C, preferably from 380° to 430°C. The upper temperature level may be from 420° to 550°C, preferably from 450° to 510°C. Thus, for example, in a toluene disproportionation process, the nominal conversion temperature may be 445°C, and the gradient selectivation method may comprise a lower temperature level of 410°C and an upper temperature level of 490°C.

[0030] The gradient selectivation procedure will generally have a duration of from 20 hr to 500 hr on stream, preferably from 50 hr to 200 hr on stream. For stepped gradients, comprising one or more intermediate temperature steps, the duration of each step may be selected independently of those of any other steps. Typically, each step will have a duration of 2 hr to 100 hr, preferably 5 hr to 75 hr. The temperature differential (the "rise") of each step may range from 1° to 50°C, preferably from 5° to 20°C. The temperature differentials for each step may be the same or different.

[0031] Despite the conventional understanding that *in situ* selectivation is useful as an adjunct to *ex situ* selectivation techniques, Applicants have unexpectedly found that a metal-functionalized catalyst can be effectively selectivated under reactor conditions including the progressive temperature gradient described herein, but without requiring any *ex situ* selectivation. As a result, the "gradient selectivation" referred to herein need not be associated with or preceded by a primary preselectivation procedure. Even so, it is possible, and may be desirable, to modify the catalyst of the invention by conducting an *ex situ* preselectivation procedure prior to the gradient selectivation described herein to further enhance conversion yields.

[0032] The organosilicon compound used to selectivate the zeolite may be a silicone, siloxane, or silane. Silicones are defined herein as those compounds wherein silicon atoms are bonded to one another via oxygen atoms. Silanes are defined herein as those compounds wherein silicon atoms are bonded directly to one another. These organosilicon compounds may have at least 2 silicon atoms per molecule. The molecular weight of the silicon compound employed as a selectivating agent may be between 80 and 20,000, and is preferably within the approximate range of 150 to 10,000. The kinetic diameter of the organosilicon selectivating agent is preferably larger than the zeolite pore diameter, to avoid entry of the selectivating agent into the zeolite pores and any concomitant reduction in the internal activity of the zeolite.

[0033] Examples of suitable organosilicon compounds for use in the gradient selectivation process of the present invention are described in U.S. Patent No. 5,498,814. Preferred organosilicon selectivating agents include dimethylphenylmethyl polysiloxane (e.g., Dow-550) and phenylmethyl polysiloxane (e.g., Dow-710). Dow-550 and Dow-710 are available from Dow Chemical Co., Midland, Michigan.

[0034] As noted previously, the molecular sieve catalyst used in the process of the invention can optionally be subjected to preselectivation prior to undergoing the gradient *in-situ* selectivation process described above. Such preselectivation typically involves exposure of the catalyst to one or more *ex situ* selectivation treatments with a silicon compound in a liquid carrier, each treatment being followed by calcination of the treated material in an oxygen-containing atmosphere, e.g., air. The silicon compound may be present in the form of a solute dissolved in the liquid carrier or in the form of emulsified droplets in the liquid carrier. A suitable preselectivation procedure is described in U.S. Patent Nos. 5,476,823 and 5,403,800.

[0035] The present catalyst may also be subjected to coke selectivation. This optional coke selectivation may involve contacting the catalyst with a thermally decomposable organic compound at an elevated temperature in excess of the decomposition temperature of the compound but below the temperature at which the crystallinity of the zeolite is adversely affected. This contact temperature may be, for example, less than 650°C.

[0036] Organic materials useful for this coke selectivation process encompass a wide variety of compounds, including by way of example, hydrocarbons, such as paraffins, cycloparaffins, olefins, cycloolefins and aromatics; oxygen-con-

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tainin organic compounds, such as alcohols, aldehydes, ethers, ketones and phenols; and heterocyclics, such as furans, thiophenes, pyrroles and pyridines. A hydrogen co-feed may be used to deter the excessive build-up of coke. Further details regarding coke selectivation techniques are provided in U.S. Patent No. 4,117,026, as well as in PCT Publication No. WO94/27934. An organosilicon co-feed may be, optionally, included along with the organic material feed used for coke selectivation. this organosilicon material may be selected from the organosilicon compounds mentioned hereinabove for use in the *in situ* selectivation of the catalyst.

Shape-Selective Hydrocarbon Conversion Processes

[0037] The functionalized catalyst according to the invention has particular utility in toluene disproportionation processes, to yield high purity *p*-xylene with ethylbenzene by-product yields that are substantially reduced over those possible using conventional processes. Operating conditions for effecting toluene disproportionation using the functionalized catalyst of the invention include a reactor inlet temperature of 350° to 540°C, preferably greater than 400°C, a pressure of 100 to 35,000 kPa (atmospheric to 5000 psig), preferably of 800 to 7000 kPa (100 to 1000 psig), a WHSV of 0.1 to 20, preferably 2 to 4, and a H₂/HC mole ratio of 0.1 to 20, preferably 2 to 4.

[0038] The modified catalysts of the invention are also advantageously used in other hydrocarbon conversion processes including as non-limiting examples: cracking hydrocarbons with reaction conditions including a temperature of 300° to 700°C, a pressure of 10 to 3,000 kPa, and a WHSV of 0.1 to 20 hr⁻¹; dehydrogenating hydrocarbon compounds with reaction conditions including a temperature of 300° to 700°C, a pressure of 10 to 1,000 kPa, and WHSV of 0.1 to 20 hr⁻¹; converting paraffins to aromatics with reaction conditions including a temperature of from 300° to 700°C, a pressure of 10 to 6,000 kPa, a WHSV of 0.5 to 400 hr⁻¹, and a H₂/HC mole ratio of 0 to 20; converting olefins to aromatics, e.g., benzene, toluene and xylene, with reaction conditions including a temperature of 100° to 700°C, a pressure of 10 to 6,000 kPa, a WHSV of 0.5 to 400 hr⁻¹, and a H₂/HC mole ratio of 0 to 20; converting alcohols, e.g., methanol, or ethers, e.g., dimethylether, or mixtures thereof to hydrocarbons including olefins and/or aromatics with reaction conditions including a temperature of 275° to 600°C, a pressure of 50 to 5,000 kPa, and a LHSV of 0.5 to 100 hr⁻¹; isomerizing xylene feedstock components with reaction conditions including a temperature of 230° to 510°C, a pressure of 300 to 3,500 kPa, a WHSV of 0.1 to 200 hr⁻¹, and a H₂/HC mole ratio of 0 to 100; alkylating aromatic hydrocarbons, e.g., benzene and alkylbenzenes in the presence of an alkylating agent, e.g., olefins, formaldehyde, alkyl halides and alcohols, with reaction conditions including a temperature of 250° to 500°C, a pressure of 100 to 20,000 kPa, a WHSV of 2 to 2,000 hr⁻¹, and an aromatic hydrocarbon/alkylating agent mole ratio of 1/1 to 20/1; and transalkylating aromatic hydrocarbons in the presence of polyalkylaromatic hydrocarbons with reaction conditions including a temperature of 340° to 500°C, a pressure of 100 to 20,000 kPa, a WHSV of 10 to 1,000 hr⁻¹, and an aromatic hydrocarbon/polyalkylaromatic hydrocarbon mole ratio of 1/1 to 16/1.

[0039] In general, therefore, catalytic conversion conditions over a catalyst comprising the modified zeolite include a temperature of 100° to 760°C, a pressure of 10 to 20,000 kPa, a WHSV of 0.08 to 2000 hr⁻¹ and a hydrogen/organic (e.g., hydrocarbon compound) mole ratio of 0 to 100.

[0040] The following examples are provided to assist in a further understanding of the invention.

EXAMPLE 1

[0041] A HZSM-5 catalyst was functionalized by adding platinum as a hydrogenation-dehydrogenation metal. A catalyst preparation was designed to yield a functionalized catalyst containing 0.05 wt.% platinum. Thirty grams (30 g) of HZSM-5 was added to 150 mL of a 1 M aqueous solution of NH₄NO₃. The pH of the mixture was adjusted to pH 8-9 with dilute NH₄OH. The mixture was then placed on an orbital stirrer and stirred for 1 hr. Then a solution of 0.0300 g tetraamine platinum(II) nitrate in 1.0 mL water as added to the mixture. The mixture was placed on an orbital stirrer and stirred overnight. The catalyst mixture was then filtered, rinsed with distilled water, and dried at 150°C for 1 hr. Finally, the functionalized catalyst (Pt-HZSM-5) was program calcined in air at 5°C/min to 350°C, then held for 3 hr at 350°C.

EXAMPLE 2

[0042] Two grams (2.0 g) of Pt-HZSM-5 catalyst prepared as described in Example 1 was *in situ* selectivated according to a conventional protocol, using a 2% solution of hexamethylcyclotrioxane in toluene. The selectivation conditions included a temperature of 447°C, a pressure of 3550 kPa (500 psig), a WHSV of 4 hr⁻¹, and H₂/HC ratio of 2. During 54 hr selectivation time, *p*-xylene selectivity increased from 24% of the xylenes (thermodynamic equilibrium proportion) to 96.4% at 30% conversion. However, over the same time on stream, ethylbenzene make increased gradually from 0.5 wt.% to 5.2 wt.% based on the total C₈ product.

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EXAMPLE 3

[0043] A 2.0 g sample of Pt-HZSM-5 catalyst prepared as described in Example 1 was gradient selectivated according to the method of the invention. In this case the gradient selectivation was performed generally in accordance with the conditions described in Example 2, except that a progressive temperature gradient was employed over the course of the selectivation period. The following stepped gradient program was used:

TABLE 1

Selectivation Temperature (°C)	Hours at Selectivation Temperature
415	48
430	45
445	53
465	22
485	6

When the gradient selectivation was complete, the temperature was lowered to 430°C and the WHSV was lowered to 3 hr⁻¹, while retaining H₂/HC = 2.

[0044] During the gradient selectivation, the *p*-xylene selectivity increased from the thermodynamic 24 wt.% of the xylenes to 98.6 wt.%, at 23% conversion. In contrast to the catalyst described in Example 2, ethylbenzene selectivity did not increase with time on stream, but actually decreased somewhat, from 0.6 to 0.4% of the C₈ product. The ethylbenzene make remained constant for 6 days on stream. Following an air regeneration procedure (1°C/min to 538°C, then hold at 538°C for 1.5 hr), conversion was resumed, using the same conversion conditions, with ethylbenzene selectivity at 0.4%. This result indicates that the functionalized catalyst according to the invention was substantially stable under conversion conditions.

EXAMPLE 4

[0045] The catalyst of the invention also improves ethylbenzene conversion processes. In this example, an unselectivated platinum-modified catalyst representative of the prior art was compared to a gradient selectivated platinum-modified catalyst of the invention. The ethylbenzene conversion was performed using a feed consisting of 20 wt.% ethylbenzene, 60 wt.% *m*-xylene, and 20 wt.% *o*-xylene. The results of this experiment are illustrated in Table 2, below. Conventional conversion conditions were used: 427°C, 1135 kPa (150 psig), and H₂/HC = 1, with WHSV as indicated in the Table.

TABLE 2

Yield (wt.%)	Prior Art	Gradient Selectivated	
	WHSV = 20	WHSV = 10	WHSV = 20
C ₅	3.6	4.7	3.4
Benzene	9.8	11.9	8.8
Toluene	2.9	0.8	0.3
Ethylbenzene	5.4	2.8	6.4
<i>p</i> -Xylene	17.0	0.1	0.1
<i>m</i> -Xylene	42.5	59.6	60.3
<i>o</i> -Xylene	18.0	20.0	20.6
C ₉ ⁺	1.0	0.0	0.0
Ethylbenzene Conversion (%)	73	86	68
Xylene Conversion (%)	3.3	0.3	<0.1
Toluene + C ₉ ⁺ (wt.%)	3.9	0.8	0.3

Compared to the test results for the non-selectivated prior art catalyst, the functionalized catalyst of the invention significantly reduced xylene loss from 3.3% to essentially zero. Also, the functionalized catalyst was effective to reduce by-products (toluene + C₉⁺) by an order of magnitude, i.e., from 3.9 to 0.3 wt.%. These results were obtained at similar ethylbenzene conversion levels (68% vs. 73%).

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[0046] Moreover, by lowering the WHSV from 20 hr⁻¹ to 10 hr⁻¹, the ethylbenzene conversion over the catalyst of the invention increased significantly to 86%. The xylene loss and by-product make each increased only slightly to 0.3% and 0.8 wt.%, respectively, but these amounts are still substantially less than those produced by the conventional catalyst.

Claims

1. A process for producing a shape-selective, metal containing catalyst comprising the steps of incorporating a hydrogenation-dehydrogenation metal into a molecular sieve catalyst to provide a metal-containing catalyst and then contacting the metal-containing catalyst *in situ* in a reactor used for subsequent hydrocarbon conversion with a feed stream comprising hydrogen and an organosilicon compound under conditions to deposit a siliceous coating on the catalyst, characterized in that said conditions comprise a progressive temperature gradient including a first temperature within the range of 350 to 460°C and a second temperature higher than said first temperature in the range of 420 to 550°C.
2. A process as claimed in claim 1, characterized in that said metal is selected from cadmium, cobalt, copper, gold, iron, mercury, molybdenum, nickel, osmium, palladium, platinum, rhodium, ruthenium, silver, zinc and mixtures thereof.
3. A process as claimed in claim 1 or claim 2, characterized in that said catalyst comprises a zeolite selected from ZSM-5, ZSM-11, ZSM-12, ZSM-22, ZSM-23, ZSM-35, ZSM-48, ZSM-57 and ZSM-58.
4. A process as claimed in any one of the preceding claims, characterized in that said first temperature is within the range of 380 to 430°C.
5. A process as claimed in any one of the preceding claims, characterized in that said second temperature is within the range of 450 to 510°C.
6. A process as claimed in any one of the preceding claims, characterized in that said feed stream also comprises a hydrocarbon.
7. A process as claimed in any one of the preceding claims, characterized in that said conditions also include a pressure of 100 to 20,000 kPa, a H₂/hydrocarbon mole ratio of 0 to 20, and a WHSV of 0.1 to 100 hr⁻¹.
8. A process as claimed in any one of the preceding claims, characterized in that the catalyst has been further modified by exposing the catalyst to at least one preselectivation sequence comprising contacting the catalyst with an organosilicon compound in a liquid carrier and then calcining the catalyst.
9. A hydrocarbon conversion process comprising characterizing by contacting a hydrocarbon feed with a shape-selective, metal-containing catalyst produced by a process as claimed in any one of the preceding claims.
10. A hydrocarbon conversion process as claimed in claim 9 characterized in that the hydrocarbon feed comprises toluene and the process includes disproportionation of the toluene to selectively produce para-xylene.

Patentansprüche

1. Verfahren zur Herstellung eines formselktiven, metallhaltigen Katalysators, umfassend die Schritte des Einführens eines Hydrierungs/Dehydrierungs-Metalls in einen Molekularsiebkatalysator, wodurch ein metallhaltiger Katalysator bereitgestellt wird, und des anschließenden Kontaktes des metallhaltigen Katalysators *in situ* in einem für die anschließende Kohlenwasserstoffumwandlung verwendeten Reaktor mit einem Beschickungsstrom, der Wasserstoff und eine Organosiliciumverbindung umfaßt, bei Bedingungen, so daß auf dem Katalysator eine siliciumhaltige Beschichtung aufgebracht wird, dadurch gekennzeichnet, daß diese Bedingungen einen progressiven Temperaturgradienten umfassen, der eine erste Temperatur im Bereich von 350 bis 460°C und eine zweite Temperatur oberhalb der ersten Temperatur im Bereich von 420 bis 550°C einschließt.
2. Verfahren nach Anspruch 1, dadurch gekennzeichnet, daß das Metall aus Cadmium, Cobalt, Kupfer, Gold, Eisen,

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Quecksilber, Molybdän, Nickel, Osmium, Palladium, Platin, Rhodium, Rhodium, Ruthenium, Silber, Zink und Gemischen davon ausgewählt ist.

3. Verfahren nach Anspruch 1 oder Anspruch 2, dadurch gekennzeichnet, daß der Katalysator einen Zeolith, ausgewählt aus ZSM-5, ZSM-11, ZSM-12, ZSM-22, ZSM-23, ZSM-35, ZSM-48, ZSM-57 und ZSM-58, umfaßt.
4. Verfahren nach einem der vorstehenden Ansprüche, dadurch gekennzeichnet, daß die erste Temperatur im Bereich von 380 bis 430°C liegt.
5. Verfahren nach einem der vorstehenden Ansprüche, dadurch gekennzeichnet, daß die zweite Temperatur im Bereich von 450 bis 510°C liegt.
6. Verfahren nach einem der vorstehenden Ansprüche, dadurch gekennzeichnet, daß der Beschickungsstrom auch einen Kohlenwasserstoff umfaßt.
7. Verfahren nach einem der vorstehenden Ansprüche, dadurch gekennzeichnet, daß die Bedingungen auch einen Druck von 100 bis 20.000 kPa, ein H₂/Kohlenwasserstoff-Molverhältnis von 0 bis 20 und eine WHSV von 0,1 bis 100 h⁻¹ einschließen.
8. Verfahren nach einem der vorstehenden Ansprüche, dadurch gekennzeichnet, daß der Katalysator außerdem modifiziert worden ist, indem der Katalysator mindestens einer Vorselektivierungssequenz ausgesetzt wurde, die den Kontakt des Katalysators mit einer Organosiliciumverbindung in einem flüssigen Träger und das anschließende Kalzinieren des Katalysators umfaßt.
9. Kohlenwasserstoffumwandlungsverfahren, dadurch gekennzeichnet, daß es den Kontakt einer Kohlenwasserstoffbeschickung mit einem formselektiven, metallhaltigen Katalysator umfaßt, der nach einem Verfahren nach einem der vorstehenden Ansprüche hergestellt worden ist.
10. Kohlenwasserstoffumwandlungsverfahren nach Anspruch 9, dadurch gekennzeichnet, daß die Kohlenwasserstoffbeschickung Toluol umfaßt und das Verfahren die Disproportionierung des Toluols einschließt, wodurch selektiv p-Xylol erzeugt wird.

Revendications

1. Procédé de production d'un catalyseur à sélectivité de forme contenant des métaux, comprenant les étapes consistant à incorporer un métal d'hydrogénation-déshydrogénation dans un catalyseur à tamis moléculaire, pour fournir un catalyseur contenant un métal, puis mettre en contact le catalyseur contenant un métal, *in situ*, d'un réacteur utilisé pour une conversion subséquente des hydrocarbures avec un courant d'alimentation comprenant de l'hydrogène et un composé organosilicé, dans des conditions permettant de déposer un revêtement silicé sur le catalyseur, caractérisé en ce que lesdites conditions comprennent un gradient de température progressif, incluant une première température dans la plage de 350 à 460°C et une deuxième température supérieure à ladite première température, dans la plage de 420 à 550°C.
2. Procédé selon la revendication 1, caractérisé en ce que ledit métal est sélectionné parmi le cadmium, cobalt, cuivre, or, fer, mercure, molybdène, nickel, osmium, palladium, platine, rhénium, rhodium, ruthénium, argent, zinc et leurs mélanges.
3. Procédé selon la revendication 1 ou la revendication 2, caractérisé en ce que ledit catalyseur comprend un zéolithe sélectionné parmi ZSM-5, ZSM-11, ZSM-12, ZSM-22, ZSM-23, ZSM-35, ZSM-48, ZSM-57 et ZSM-58.
4. Procédé selon l'une quelconque des revendications précédentes, caractérisé en ce que ladite première température est dans la plage de 380 à 430°C.
5. Procédé selon l'une quelconque des revendications précédentes, caractérisé en ce que ladite deuxième température est dans la plage de 450 à 510°C.
6. Procédé selon l'une quelconque des revendications précédentes, caractérisé en ce que ledit courant d'alimen-

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tation comprend également un hydrocarbure.

- 5 7. Procédé selon l'une quelconque des revendications précédentes, caractérisé en ce que lesdites conditions comprennent également une pression de 100 à 20.000 kPa, un rapport molaire H_2 /hydrocarbure de 0 à 20, et un WHSV de 0,01 à 100 heures⁻¹.
- 10 8. Procédé selon l'une quelconque des revendications précédentes, caractérisé en ce que le catalyseur a été en outre modifié par exposition du catalyseur à au moins une séquence de présélection, comprenant la mise en contact du catalyseur avec un composé organosilicé et un porteur liquide, puis calcination du catalyseur.
- 15 9. Procédé de conversion d'hydrocarbures, caractérisé par la mise en contact de l'alimentation en hydrocarbure avec un catalyseur à sélectivité de forme et contenant un métal, produit par un procédé selon l'une quelconque des revendications précédentes.
- 20 10. Procédé de conversion d'hydrocarbures selon la revendication 9, caractérisé en ce que l'alimentation en hydrocarbure comprend du toluène et le procédé comprend la dissipation du toluène, afin de produire sélectivement du para-xylène.
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